

Author	PSF	Ngals (o)	% stars	% false	Ngals (m)	mean mag (o)	% mag dec	$\langle e_1^s \rangle$ (o)	$\langle e_2^s \rangle$ (o)	$\langle e_1^s \rangle$ (m)	$\langle e_2^s \rangle$ (m)
HH	A	28	0	0	26	14.35	0.3	-0.003 ± 0.004	0.004 ± 0.004	-0.004 ± 0.004	0.006 ± 0.004
HH	B	24	0	0	23	14.24	0.4	-0.001 ± 0.003	0.000 ± 0.003	0.000 ± 0.003	0.000 ± 0.004
HH	C	24	0	0	22	14.27	0.4	-0.003 ± 0.004	0.006 ± 0.005	-0.003 ± 0.004	0.006 ± 0.005
HH	D	26	1	0	24	14.22	0.4	0.000 ± 0.004	0.001 ± 0.004	0.000 ± 0.004	0.001 ± 0.005
HH	E	26	1	0	24	14.22	0.4	0.000 ± 0.004	0.001 ± 0.004	0.000 ± 0.004	0.001 ± 0.005
HH	F	26	1	0	24	14.21	0.4	0.000 ± 0.004	0.001 ± 0.004	0.000 ± 0.004	0.001 ± 0.005
MJ	A	27	0	0	24	14.58	0.4	-0.003 ± 0.003	0.001 ± 0.003	-0.003 ± 0.003	0.003 ± 0.003
MJ	B	26	0	0	23	14.32	0.6	-0.001 ± 0.003	0.002 ± 0.003	-0.001 ± 0.003	0.002 ± 0.003
MJ	C	25	0	0	22	14.56	0.6	-0.004 ± 0.003	0.003 ± 0.003	-0.003 ± 0.003	0.004 ± 0.003
MJ	D	27	0	0	24	14.48	0.6	0.000 ± 0.003	0.002 ± 0.003	0.000 ± 0.003	0.002 ± 0.003
MJ	E	27	0	0	24	14.48	0.6	-0.001 ± 0.003	0.001 ± 0.003	-0.002 ± 0.003	0.001 ± 0.003
MJ	F	27	0	0	24	14.49	0.6	-0.001 ± 0.003	0.002 ± 0.003	-0.001 ± 0.003	0.002 ± 0.003
J2	A	27	0	0	24	13.87	0.1	-0.001 ± 0.006	0.006 ± 0.007	-0.001 ± 0.006	0.008 ± 0.007
J2	B	26	0	0	23	13.74	0.2	0.000 ± 0.004	-0.002 ± 0.005	0.001 ± 0.004	-0.001 ± 0.005
J2	C	25	0	0	22	13.78	0.4	-0.006 ± 0.007	0.006 ± 0.007	-0.007 ± 0.007	0.007 ± 0.008
J2	D	27	0	0	24	13.70	0.1	0.001 ± 0.006	-0.002 ± 0.007	0.001 ± 0.006	-0.002 ± 0.007
J2	E	27	0	0	24	13.70	0.1	0.001 ± 0.006	-0.002 ± 0.006	0.001 ± 0.007	-0.002 ± 0.007
J2	F	27	0	0	24	13.72	0.2	0.001 ± 0.006	-0.002 ± 0.006	0.001 ± 0.006	-0.002 ± 0.007
KK	A	32	0	0	26	14.74	0.7	-0.003 ± 0.003	0.002 ± 0.004	-0.004 ± 0.004	0.004 ± 0.004
KK	B	28	0	0	21	14.71	0.9	-0.001 ± 0.003	0.001 ± 0.003	-0.001 ± 0.004	0.001 ± 0.004
KK	C	27	0	0	21	14.65	0.9	-0.005 ± 0.004	0.003 ± 0.004	-0.006 ± 0.004	0.003 ± 0.005
KK	D	29	1	0	23	14.59	0.8	0.002 ± 0.004	0.000 ± 0.004	0.002 ± 0.004	-0.001 ± 0.004
KK	E	29	1	0	23	14.58	0.8	0.002 ± 0.004	0.000 ± 0.004	0.003 ± 0.004	-0.001 ± 0.004
KK	F	29	0	0	23	14.58	0.8	0.001 ± 0.004	0.000 ± 0.004	0.002 ± 0.004	-0.001 ± 0.004
RM	A	36	0	0	32	14.70	0.6	-0.001 ± 0.003	0.002 ± 0.003	-0.002 ± 0.003	0.003 ± 0.003
RM	B	35	0	0	31	14.51	0.5	-0.002 ± 0.003	0.000 ± 0.003	-0.002 ± 0.003	0.001 ± 0.003
RM	C	27	0	0	22	14.52	0.9	-0.003 ± 0.004	0.006 ± 0.004	-0.003 ± 0.004	0.007 ± 0.004
RM	D	32	0	0	28	14.54	0.8	-0.002 ± 0.003	0.001 ± 0.004	-0.001 ± 0.004	0.001 ± 0.004
RM	E	32	0	0	28	14.54	0.8	-0.002 ± 0.003	0.001 ± 0.004	-0.002 ± 0.004	0.001 ± 0.004
RM	F	31	0	0	27	14.52	0.8	-0.002 ± 0.003	0.001 ± 0.004	-0.002 ± 0.004	0.001 ± 0.004

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RN	A	17	0	1	15	14.31	0.8	-0.001 ± 0.003	0.001 ± 0.003	-0.001 ± 0.004	0.003 ± 0.004
RN	B	18	0	0	15	13.99	0.8	0.000 ± 0.003	0.003 ± 0.003	0.000 ± 0.003	0.003 ± 0.003
RN	C	10	0	1	8	14.18	1.2	0.002 ± 0.005	0.002 ± 0.005	0.003 ± 0.005	0.003 ± 0.005
RN	D	16	0	1	13	14.13	0.8	-0.002 ± 0.004	0.002 ± 0.004	-0.002 ± 0.004	0.003 ± 0.004
RN	E	16	0	1	13	14.12	0.8	-0.001 ± 0.004	0.001 ± 0.004	-0.002 ± 0.004	0.003 ± 0.004
RN	F	14	0	1	11	14.08	1.0	0.000 ± 0.004	0.003 ± 0.004	-0.001 ± 0.004	0.003 ± 0.004
MS	A	43	0	1	39	14.97	0.4	-0.002 ± 0.003	-0.001 ± 0.003	-0.003 ± 0.003	0.001 ± 0.003
MS	B	40	0	1	36	14.37	0.5	-0.001 ± 0.003	-0.001 ± 0.003	-0.001 ± 0.003	-0.001 ± 0.003
MS	C	37	0	1	33	14.85	0.4	-0.005 ± 0.003	0.005 ± 0.003	-0.005 ± 0.003	0.005 ± 0.003
MS	D	39	0	1	35	14.74	0.5	0.000 ± 0.003	-0.001 ± 0.003	-0.001 ± 0.003	-0.001 ± 0.003
MS	E	39	0	1	35	14.76	0.5	0.000 ± 0.003	-0.001 ± 0.003	0.000 ± 0.003	-0.002 ± 0.003
MS	F	39	0	1	35	14.75	0.4	0.000 ± 0.003	-0.001 ± 0.003	0.000 ± 0.003	-0.001 ± 0.003
S2	A	41	0	1	36	14.75	0.2	-0.002 ± 0.003	0.000 ± 0.004	-0.003 ± 0.003	0.002 ± 0.004
S2	B	38	0	1	33	13.97	0.3	-0.001 ± 0.004	-0.001 ± 0.004	-0.001 ± 0.004	-0.001 ± 0.004
S2	C	35	0	1	30	14.57	0.3	-0.003 ± 0.004	0.007 ± 0.005	-0.003 ± 0.004	0.007 ± 0.005
S2	D	37	0	1	32	14.43	0.3	-0.003 ± 0.004	-0.003 ± 0.004	-0.003 ± 0.004	-0.003 ± 0.004
S2	E	37	0	1	32	14.43	0.3	-0.001 ± 0.004	-0.004 ± 0.004	-0.001 ± 0.004	-0.004 ± 0.004
S2	F	37	0	1	32	14.39	0.3	-0.001 ± 0.004	-0.003 ± 0.004	-0.001 ± 0.004	-0.003 ± 0.004
JB	A	37	0	0	25	15.34	1.9	-0.002 ± 0.002	-0.002 ± 0.002	-0.001 ± 0.003	-0.001 ± 0.003
JB	B	35	0	0	27	15.02	1.6	0.000 ± 0.003	0.000 ± 0.003	-0.001 ± 0.003	0.000 ± 0.003
JB	C	28	0	0	21	14.80	1.5	-0.004 ± 0.003	0.003 ± 0.003	-0.004 ± 0.004	0.004 ± 0.004
JB	D	31	0	0	23	14.84	1.8	-0.002 ± 0.003	0.000 ± 0.003	-0.002 ± 0.003	-0.001 ± 0.004
JB	E	32	1	0	24	14.85	1.7	-0.002 ± 0.003	0.000 ± 0.003	-0.003 ± 0.003	-0.001 ± 0.004
JB	F	31	1	0	23	14.84	1.7	-0.002 ± 0.003	-0.001 ± 0.003	-0.003 ± 0.003	-0.001 ± 0.004
SP	A	27	0	11	15	14.42	0.7	-0.008 ± 0.006	0.006 ± 0.006	-0.008 ± 0.007	0.008 ± 0.007
SP	B	25	0	10	14	14.40	0.8	0.001 ± 0.004	0.005 ± 0.005	0.000 ± 0.005	0.006 ± 0.006
SP	C	25	1	9	13	14.39	0.7	-0.006 ± 0.006	0.000 ± 0.007	-0.007 ± 0.007	-0.003 ± 0.009
SP	D	23	1	9	11	14.25	1.0	-0.001 ± 0.007	0.007 ± 0.007	-0.001 ± 0.009	0.012 ± 0.009
SP	E	25	1	9	14	14.29	0.8	0.000 ± 0.006	0.006 ± 0.006	0.000 ± 0.008	0.009 ± 0.008
SP	F	25	1	9	14	14.28	0.6	0.002 ± 0.006	0.006 ± 0.006	0.001 ± 0.007	0.009 ± 0.008

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TS	A	40	0	0	36	15.03	0.7	-0.002 ± 0.003	0.000 ± 0.003	-0.002 ± 0.003	0.002 ± 0.003
TS	B	37	0	0	33	15.00	0.9	-0.001 ± 0.003	-0.001 ± 0.003	-0.001 ± 0.003	-0.001 ± 0.003
TS	C	34	0	0	30	14.93	0.9	-0.005 ± 0.003	0.004 ± 0.003	-0.006 ± 0.003	0.005 ± 0.003
TS	D	36	0	0	32	14.90	0.9	0.001 ± 0.003	0.000 ± 0.003	0.001 ± 0.003	0.000 ± 0.003
TS	E	37	0	0	33	14.91	0.9	0.001 ± 0.003	0.000 ± 0.003	0.001 ± 0.003	0.000 ± 0.003
TS	F	37	0	0	32	14.90	0.9	0.001 ± 0.003	0.000 ± 0.003	0.001 ± 0.003	0.000 ± 0.003
MH	A	38	0	0	35	14.97	0.7	-0.001 ± 0.003	0.000 ± 0.003	-0.002 ± 0.003	0.002 ± 0.003
MH	B	36	0	0	32	14.91	0.7	-0.001 ± 0.003	-0.001 ± 0.003	-0.001 ± 0.003	-0.001 ± 0.003
MH	C	33	0	0	29	14.86	0.8	-0.005 ± 0.003	0.004 ± 0.003	-0.006 ± 0.003	0.005 ± 0.003
MH	D	35	0	0	31	14.82	0.7	0.001 ± 0.003	0.000 ± 0.003	0.001 ± 0.003	0.000 ± 0.003
MH	E	35	0	0	32	14.83	0.8	0.001 ± 0.003	0.000 ± 0.003	0.001 ± 0.003	0.000 ± 0.003
MH	F	35	0	0	31	14.82	0.8	0.001 ± 0.003	0.000 ± 0.003	0.000 ± 0.003	0.000 ± 0.003
ES	A	50	0	2	42	15.26	1.0	-0.002 ± 0.002	-0.001 ± 0.002	-0.003 ± 0.002	0.001 ± 0.003
ES	B	49	0	3	39	15.16	1.1	-0.001 ± 0.002	0.000 ± 0.002	-0.002 ± 0.003	0.000 ± 0.003
ES	C	45	0	2	36	15.16	1.1	-0.006 ± 0.002	0.003 ± 0.003	-0.006 ± 0.003	0.004 ± 0.003
ES	D	47	0	2	39	15.10	1.1	0.000 ± 0.002	0.000 ± 0.003	0.001 ± 0.003	-0.001 ± 0.003
ES	E	46	0	2	38	15.09	1.1	0.000 ± 0.002	0.000 ± 0.003	0.000 ± 0.003	0.000 ± 0.003
ES	F	48	1	2	39	15.10	1.1	0.000 ± 0.002	0.000 ± 0.003	0.001 ± 0.003	-0.001 ± 0.003

Table 1: Table to compare the different number density of selected sources per square arcmin, Ngals (o), and the percentage of stellar contamination (% stars) and false detections (% false) in each authors' original catalogue. The STEP2 analysis method relies on matching the original and rotated catalogues. The match introduces an effective signal-to-noise cut on the original catalogues, slightly reducing the number density of selected sources per square arcmin, Ngals (match), and decreasing the mean magnitude, column 7 (mean mag (o)) by column 8 (% dec mag). The STEP2 method does not appear to introduce any selection bias, which can be seen by comparing the mean source ellipticity $\langle e_i^s \rangle$ in the original catalogues (columns 9& 10) with the mean source ellipticity $\langle e_i^s \rangle$ in the matched catalogues (columns 11& 12)